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East Sussex County Council Transport and Environment

Bexhill to Hastings Link Road S03 Woodsgate Park Overbridge Approval in Principle

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S03 Woodsgate Park AIP

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1. HIGHWAY DETAILS

1.1 Type of highway

Over - Woodsgate Park single carriageway urban highway 6.100m width + 2 x 2.000m footways and a 1.000m wide raised area to accommodate a badger crossing

alongside the north parapet.

Under - Bexhill to Hastings Link Road - single carriageway urban all purpose road,

approximately 7.300m wide with 2.500m (min) verge on east and west sides.

1.2 Permitted traffic speed

Over:

30 mph

Under: 30 mph

1.3 Existing restrictions

The existing bridge is a single span steel beam and brick jack arch deck on brick abutments. The clear span between abutments is approximately 8.2m. The clear width between existing brick parapets is 12.5m. The bridge deck and East abutment are to be demolished.

2. SITE DETAILS

2.1 Obstacles crossed

Single carriageway urban highway over Bexhill to Hastings Link Road with Egerton Stream storm overflow pipe culvert under western verge of BHLR

3. PROPOSED STRUCTURE

3.1 Description of structure

Single span simply supported bridge on abutments with 2.000m wide verges, 6.100m wide carriageway and 1.000m wide raised adjacent to the north parapet. Overall deck width approximately 12.300m square. The existing mass brick West Abutment And wing walls are to be retained as part of the new bridge.

The structure is located at OS grid reference is 573939.400E, 108529.000N

3.2 Structural type

The structural type will be a single span simply supported bridge of steel/concrete composite construction, consisting of 7 longitudinal painted steel girders with an insitu reinforced concrete deck slab supported on bearings at the abutments. The girders are of constant depth and will be braced together with transverse bracing sets at the supports and at intermediate locations.

The superstructure will include provision of a badger tunnel adjacent to the North parapet

The East Abutment and wing walls will be brick clad reinforced concrete.

The existing masonry West Abutment is to be retained. A new reinforced concrete bearing shelf will be cast on top of the existing masonry which will be removed down to a suitable level.

3.3 Foundation type

The East Abutment and its wingwalls will be founded on reinforced concrete spread footings.

The existing mass gravity West Abutment is founded on spread footings. Strengthening works for the abutment toe are proposed if necessary.

3.4 Span arrangements

Clear square span

14.0 m

Skew angle

zero

3.5 Articulation arrangements

The deck is supported on bearings on each support with fixity being provided at the east abutment by a fixed bearing. Horizontal restraint will be provided by a guide bearing located at the West Abutment. The remaining bearings on each support will be free sliding bearings which will allow for all round movement and rotation.

An expansion joint will be provided in the carriageway construction at the West Abutment. A buried joint will be provided in the carriageway construction at the East Abutment.

3.6 Types of road restraint systems

Parapets on the bridge deck will provide normal containment level N2, a working width not greater than W4 and minimum height of 1.0m. Parapets will be of reinforced concrete construction with steeple copings and brickwork facing to both sides.

3.7 Proposed arrangements for maintenance and inspection

3.7.1 Traffic management

Traffic management will be required on the link road to enable inspection and maintenance of the deck soffit, bearings, abutment and wing wall faces and external parapet faces

3.7.2 Access

The road side faces of the parapets will be accessible for inspection and maintenance from the BHLR verges.

Access to other deck elements and pier bearings can be from a mobile access platform sited on the carriageway under the bridge.

The interior faces of the piped badger passage in the bridge deck and the buried passages under the approaches will not be accessible for inspection other than by CCTV or similar techniques.

Personnel access to the structure is via the Bexhill to Hastings Link Road under and Woodsgate Park over.

Bearings at the abutments will be set on plinths as necessary to provide 600mm minimum clearance between the beam soffit and bearing shelves for inspection and maintenance purposes.

Jacking points will be provided between all permanent bearing positions. The bridge will be designed to carry full HA design load during bearing replacement.

3.8.1 Materials and finishes

Refers to new construction only and not to elements of the existing structure retained in new works

Concrete	Element		Limiting Exposure Class
C40/50	Deck slab	top	XC3
		soffit	XD1
C40/50	Parapets including coping	gs	XD3
C40/50	Abutment and wing walls	-	XD3
C40/50	Foundations		XD3
Reinforceme			nt to be grade 500B or 500C to BS 4449:2005.

Structural steelwork

Generally Grade S355 J2 +N to EN 10025 except

as follows:

Grade S355 K2 +N to specific bottom flange

areas as noted on the drawings.

Parapets Reinforced concrete

Brick facing; reclaimed bricks from existing

structure or similar

Fill

East Abutment and wing walls West Abutment and wing walls Class 6N or 6P in accordance with the SHW Compact lightweight expanded clay aggregate fill

replacement of existing embankment fill.

Concrete finishes

Top of deck slab and bearing shelf floor U4 to receive bridge deck waterproofing

Hidden and buried surfaces F1 / U1

Deck soffit between main beams Permanent formwork (GRP)

Deck soffit (elsewhere) F2

Parapet, exposed faces F3

Protection

The top deck surface between parapet interfaces will be protected with a proprietary spray applied bridge deck waterproofing system to SHW CI 2003.

All accessible concrete surfaces greater than 150mm below finished ground level to receive waterproofing to below ground concrete surfaces in accordance with the SHW CI 2004.

3.8.2 Sustainability issues

Re-use of masonry units from the existing bridge is proposed where possible where these can be recovered in a usable condition.

3.9 Risks and hazards considered

Future excavation for maintenance or replacement of Egerton Brook storm by-pass pipe culvert under the western verge of BHLR may compromise stability of the bridge west abutment.

Standard construction methods are anticipated with normally associated risks and hazards. A design hazard log and risk assessment process is active for the scheme.

3.10 Estimated cost of proposed structure together with other structural forms considered and the reasons for their rejection including comparative whole-life costs with dates of estimates.

Other structural forms were discussed and appraised in Amey report number 262701/012 'Bexhill to Hastings Link Road, Preliminary Design, Structures Options Report' and the addendum to it numbered 262701/060

3.11 Proposed arrangements for construction

3.11.1 Traffic management

Full road closure required during construction. All vehicular and pedestrian traffic will be diverted along Buxton Drive, the A269 Ninfield Road and London Road to the north or Down Road, King Offa Way and London Road to the south. Construction of Woodsgate Park and Ninfield Road bridges to be phased such that at least one bridge is open to vehicular and pedestrian traffic at all times.

3.11.2 Service diversions

Existing low voltage and high voltage electric cables, and fibre optic telecom cables will be provided for by ducts in footways of the new structure. Details of the works/diversions of the services are being undertaken directly by the contractor and are not itemised.

The existing Egerton Stream culvert beneath the eastern zone of the highway corridor and behind the eastern wing walls of the bridge is to be replaced as part of the scheme.

3.11.3 Interface with existing structures

The existing structure will be demolished except for its West Abutment which is to be retained and re-used. The existing embankment fill to the West Abutment and wing walls will be removed and replaced with lightweight expanded clay aggregate fill to reduce lateral earth pressures. The existing bearing shelf will be removed and replaced with a new reinforced concrete bearing shelf incorporating bearing plinths. Local modification of the brick abutment may be required to accommodate the depth of the new bearing shelf.

4. DESIGN CRITERIA

4.1 Live loading, headroom

4.1.1 Loading relating to normal traffic under AW regulations and C&U regulations

Full HA loading in accordance with BD 37/01

4.1.2 Loading relating to General Order traffic under STGO regulations

30 units of HB loading in accordance with BD 37/01

4.1.3 Footway or footbridge live loading

Footway loading in accordance with BD 37/01.

4.1.4 Loading relating to Special Order Traffic, provision for exceptional abnormal loads or indivisible loads, including location of vehicle track on deck cross-section

None

4.1.5 Any special loading not covered above

Vehicle collision loading (BD 60/04)

4.1.6 Heavy or high load route requirements and arrangements being made to preserve the route, including any provision for future heavier loads or future widening.

No provision required for heavy or high loads

4.1.7 Minimum headroom provided

A minimum headroom of 5.3m will be provided to the BHLR after allowing for deflections arising from dead load, live load and settlement.

4.1.8 Authorities consulted and any special conditions required

Authority consulted

Special requirement

East Sussex CC

None

A badger passage will be provided within the bridge deck with pipe passages connecting to the cutting/embankment slopes from the wing walls near each corner of the site

4.2 List of relevant documents from the TAS

Refer to Appendix A

4.2.1 Additional relevant standards

BS 8500; Part 1; 2006	Concrete; Complementary British Standard to BS EN 206-1; Method of specifying and guidance for the specifier
BS 8500; Part 2; 2006	Concrete; Complementary British Standard to BS EN 206-1; Specification for constituent materials and concrete
BS 6779; Part 2; 1991	Specification for vehicle containment parapets of concrete construction
CHE Memorandum 227/08	The Impregnation Of Reinforced and Prestressed Concrete Highway Structures Using Hydrophobic Pore Lining Impregnants
MCDHW, Volume 1	Specification for Highway Works 1998, including amendments to November 2009
MCDHW, Volume 2	Notes for Guidance on the Specification for Highway Works 1998, including amendments to November 2009
MCDHW, Volume 3	Highway Construction Details 1991, including amendments to November 2008

4.3 Proposed Departures from Standards given in 4.2 and 4.2.1

Departure D3: Verges over/under Structures

See Appendix E

4.4 Proposed methods for dealing with aspects not covered by Standards in 4.2 and 4.2.1

Not applicable

STRUCTURAL ANALYSIS

5.1 Methods of analysis proposed for superstructure, substructure and foundations

The deck is to be analysed by plane linear elastic grillage analysis using LUSAS or SUPERSTRESS software for vertical loads, assuming simple supports. Deck analysis to cover all temporary and permanent stages of construction including the effects of formwork used for deck cantilever construction but excluding beam lifting condition.

Analysis of deck slab for local effects to be carried out using a metre strip or Pucher chart method assuming that the slab is one way spanning and continuous over main girders.

The East Abutment and wing walls are to be analysed assuming that vertical load carrying elements cantilever from foundations.

The stability of the modified existing West Abutment and wing walls will be analysed statically as a mass gravity wall using manual methods.

5.2 Description and diagram of idealised structure to be used for analysis.

See Appendix D

5.3 Assumptions intended for calculation of structural element stiffness

Element stiffness for composite steel / concrete members will be determined in accordance with BS5400; Part 3-2000 as implemented by BD 13/06, Part 4-1990 as implemented by BD 24/92 and Part 5-2005 as implemented by BD 16/82.

Element stiffness for concrete members will be determined in accordance with BS5400; Part 4; 1990; Clause 4.4 using full elastic uncracked member cross sections ignoring.

Global member stiffness for analysis will be determined as either composite or non-composite as appropriate to the construction or permanent stage under consideration.

Model layout will be based on the recommendations given in 'Bridge Deck Behaviour, Second Edition' by E.C. Hambly.

5.4 Proposed earth pressure coefficients (k_a , k_0 , or k_p) to be used in the design of earth retaining elements

For the analysis of earth retaining elements, k_a will be used for stability calculations and k_0 for structural element design (calculated in accordance with BD 30/87).

For the 6N/6P backfill to the east abutment, a representative peak angle of friction of 36° will be used, for which $k_a = 0.26$; $k_p = 3.85$ and $k_0 = 0.41$.

For the 6T backfill to the west abutment, a representative peak angle of friction of 37° will be used, for which $k_a = 0.25$; $k_p = 4.02$ and $k_0 = 0.40$.

6. GEOTECHNICAL CONDITIONS

6.1 Acceptance of recommendations of Section 8 of the Geotechnical Report to be used in the design and reasons for any proposed changes.

Section 2 of the Geotechnical Report has not been completed at this stage.

6.2 Geotechnical Report Highway Structure Summary Information

A draft Geotechnical Report Highway Structure Summary sheet based on the information available in Part 1 of the Geotechnical Report is attached in Appendix C. A full Geotechnical Report Highway Structure Summary sheet and extracts from the completed Geotechnical Report Section 2 will be produced following development of the Geotechnical Report.

6.3 Differential settlement to be allowed for in the design of the structure.

25mm between adjacent supports:
20mm between structure and approach embankment (within 10 metres of the interface)

6.4 If the Geotechnical Report is not yet available, state when the results are expected and list the sources of information used to justify the preliminary choice of foundations.

The preliminary choice of foundation is discussed in the draft Geotechnical Report Highway Structure Summary sheet contained in Appendix C. Part 2 of the Geotechnical Report, including Section 2 Highway Structures, is expected to be completed in Phase 2 of the project.

7. CHECKING

7.1 Proposed category of structure

Category 2

7.2 If Category 3, name of proposed Independent checkers.

Not applicable

7.3 Erection proposals or temporary works for which an independent check will be required, listing parts of the structure affected with reasons for recommending an independent check.

None

8. DRAWINGS AND DOCUMENTS

8.1 List of drawings and documents accompanying the submission.

Appendix A TAS dated February 2009

Appendix B <u>Drawing No</u> <u>Title</u>

B1297000-PH1/1600.01a/9031 Woodsgate Park Overbridge

General Arrangement

Appendix C Geotechnical Information

Appendix D Idealised Structure

Appendix E Departures from Standards

9	THE ABOVE IS SUBMITTED FOR ACCEPTANCE
9.1	Signed Name: P Goodchild Position: Structures team leader, Jacobs Engineering Qualifications: BSc, CEng, MICE, MIStructE
	Date 3 September 2012
9.2	Endorsement by contractor
	Signed 1
	Name: S. LAPTHORN
	Engineering qualifications: Many (Hons) Cany MICE
	Engineering qualifications: Many (Hons) Cong MICE Position: Design Concording Hondow, Hochtief Vinci Joint Venture
	Date: 10/09/12.
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10.	THE ABOVE IS REJECTED/AGREED SUBJECT TO THE AMENDMENTS AND CONDITIONS SHOWN BELOW.
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10.	SHOWN BELOW. Reviewed
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Appendix A List of Relevant Documents

Schedule of Design Documents Relating to Highway Bridges and Structures; February 2009

British Standards

BS 5268; Part 2; 2002	Structural Use of Timber		
BS 5400	Steel concrete and composite bridges		
Part 1; 1988	General Statement (see BD 15)		
Part 2; 1978	Specification for loads (see BD 14)		
Part 3; 2000	CP for design of steel bridges (see BD 13)		
Part 4; 1990	CP for design of concrete bridges (see BD 24)		
Part 5; 1979	CP for design of composite bridges (see BD 16)		
Part 9; 1983	Bridge bearings (see BD 20)		
Part 10; 1980	CP for fatigue (see BD 9)		
BS 5628; Part 1; 1992	Unreinforced Masonry		
BS 5930; 1999	Site Investigations		
BS 6031; 1981	Earthworks		
BS 8002; 1994	Earth retaining structures		
BS 8004; 1986	Foundations		
BS-8118; 1991	The structural use of aluminium		
BS EN 1317-1-1998; Road Restraint Systems – Part 1	Terminology and general criteria for test methods		
BS EN 1317-2-1998; Road Restraint Systems – Part 2	Performance classes, impact test acceptance criteria and test methods for safety barriers		
BS EN 1317-3-2000; Road Restraint Systems Part 3	Performance classes, impact test acceptance criteria and test methods for crash-cushions		
DD ENV 1317-4-2002; Road Restraint Systems – Part 4	Terminals and transitions		
BS-EN-14388; 2005	Road traffic noise reducing devices - Specification		

Miscellaneous

Circular Roads No 61/72 - Routes for heavy and high abnormal loads.

Railway Group Approved Code of Practice GC/RC5510: Recommendations for the Design of Bridges (2000) (for full list of other Network Rail Standards, refer to RSSB, Railway Safety and Standards Board)

Simplified Tables of External Loads on Buried Pipelines (1986)

Traffic Management Act 2004

The Manual of Contract Documents for Highway Works (MCDHW)

Volume 1: Specification for Highway Works 1998, including amendments to November 2007

Volume 2: Notes for Guidance on the Specification for Highway Works 1998, including amendments to

November 2007

Volume 3: Highway Construction Details 1991, including amendments to May 2007

The Design Manual for Roads and Bridges (DMRB)

Bridges and Structures (BA Series) Reproduced on following pages

Bridges and Structures (BD Series)

Reproduced on following pages

Bridges and Structures, Technical Memoranda (BE Series)

Reproduced on following pages

Traffic Engineering and Control, Standards (TD Series)

TD 9/93 Road layout and geometry. Highway link design

TD 19/06 Requirement of Road Restraint Systems & correction No. 1

TD 27/05 Cross Sections and headroom

TD 36/93 Subways for pedestrians and cyclists, layout and dimensions

Highways, Advice Notes (HA Series)

HA 59/92 Mitigating Against Effects on Badgers

HA 80/99 Nature Conservation Advice in Relation to Bats

HA 84/01 (1) Nature Conservation and Biodiversity

HA-97/01 Nature Conservation Management Advice in Relation to Dormice

HA 98/01 Nature Conservation Management Advice in Relation to Amphibians

Highways, Standards (HD Series)

HD 22/08 Managing Geotechnical Risk

BA-9/81	ADVICE NOTES - BRIDGES AND STRUCTURES (BA SERIES) The Use of BS 5400: Part 10: 1980. Code of Practice for Fatigue Amendment No. 1
BA-16/97	The Assessment of Highway Bridges and Structures. Amendment No. 1 Amendment No.2
BA 19/85	The Use of BS 5400: Part 3: 1982
BA 24/87	Early Thermal Cracking of Concrete Amendment No. 1
BA 26/94	Expansion Joints for Use in Highway Bridge Decks
BA 28/92	Evaluation of Maintenance Costs in Comparing Alternative Designs for Highway Structures
BA-30/94	Strengthening of Concrete Highway Structures Using Externally Bonded Plates
BA-34/90	Technical Requirements for the Assessment and Strengthening Programme for Highway Structures
BA-35/90	Inspection and Repair of Concrete Highway Structures
BA 36/90	The Use of Permanent Formwork
BA 37/92	Priority Ranking of Existing Parapets
BA 38/93	Assessment of the Fatigue Life of Corroded or Damaged Reinforcing Bars
BA 39/93	Assessment of Reinforced Concrete Half-joints
BA-40/93	Tack Welding of Reinforcing Bars
BA 41/98	The Design and Appearance of Bridges
BA 42/96	The Design of Integral Bridges [Incorporating Amendment No. 1 dated May 2003]
BA-43/94	Strengthening, Repair and Monitoring of Post-tensioned Concrete Bridge Decks
BA-44/96	Assessment of Concrete Highway Bridge and Structures
BA 47/99	Waterproofing and Surfacing Concrete Bridge Decks
BA 50/93	Post-tensioned Concrete Bridges: Planning, Organisation and Methods for Carrying Out Special Inspections
BA 51/95	The Assessment of Concrete Structures Affected by Steel Corrosion
BA 52/94	The Assessment of Concrete Highway Structures Affected by Alkali Silica Reaction
BA 53/94	Bracing Systems and the Use of U-Frames in Steel Highway Bridges
BA 54/94	Load Testing for Bridge Assessment
BA-55/06	The Assessment of Bridge Substructures and Foundations, Retaining Walls and Buried Structures
BA 56/96	The Assessment of Steel Highway Bridges and Structures
BA 57/01	Design for Durability
BA 58/94	Design of Bridges and Concrete Structures with External Unbonded Prestressing
BA 59/94	Design of Highway Bridges for Hydraulic Action
BA 61/96	The Assessment of Composite Highway Bridges
BA 67/96	Enclosure of Bridges
BA 68/97	Crib Retaining Walls
BA 72/03	Maintenance of Road Tunnels

BA-74/06	ADVICE NOTES - BRIDGES AND STRUCTURES (BA SERIES) Assessment of Scour at Highway-Bridges
BA 80/99	Use of Rock Bolts
BA 82/00	Formation of Continuity Joints in Bridge Decks
BA 83/02	Cathodic Protection for Use in Reinforced Concrete Highway Structures
BA 84/02	Use of Stainless Steel Reinforcement in Highway Structures
BA-85/04	Coatings for Concrete Highway Structures & Ancillary Structures
BA-86//06	Advice Notes on the Non-Destructive Testing of Highway Structures
BA-87//04	Management of Corrugated Steel Buried Structures
BA-88//04	Management of Buried Concrete Box Structures
BA 92/07	The Use of Recycled Concrete Aggregates in Structural Concrete
BA-93/09	Structural Assessment of Bridges with Deck Hinges
	STANDARDS - BRIDGES AND STRUCTURES (BD SERIES)
BD 2/05	Technical Approval of Highway Structures
BD-7/01	Weathering Steel for Highway Structures
BD 9/81	Implementation of BS 5400: Part 10: 1980. Code of Practice for Fatigue
BD-10/97	Design of Highway Structures in Areas of Mining Subsidence
BD-12/01	Design of Corrugated Steel Buried Structures with Spans-Greater than 0.9 Metres and up to 8.0 Metres
BD-13/06	Design of Steel Bridges. Use of BS 5400: Part 3: 2000
BD 15/92	General Principles for the Design and Construction of Bridges. Use of BS 5400: Part 1: 1988
BD 16/82	Design of Composite Bridges. Use of BS 5400: Part 5: I979 Amendment No. 1
BD 20/92	Bridge Bearings. Use of BS 5400: Part 9: 1983
BD 21/01	The Assessment of Highway Bridges and Structures
BD 24/92	Design of Concrete Bridges. Use of BS 5400: Part 4: 1990
BD-27/86	Materials for the Repair of Concrete Highway Structures
BD 28/87	Early Thermal Cracking of Concrete Amendment No. 1
BD 29/04	Design Criteria for Footbridges
BD 30/87	Backfilled Retaining Walls and Bridge Abutments
BD 31/01	The Design of Buried Concrete Box and Portal Frame Structures
BD 33/94	Expansion Joints for Use in Highway Bridge Decks
BD 34/90	Technical Requirements for the Assessment and Strengthening Programme for Highway Structures
BD 35/06	Quality-Assurance-Scheme for Paints and Similar Protective Coatings
BD 36/92	Evaluation of Maintenance Costs in Comparing Alternative Designs for Highway Structures
BD 37/01	Loads for Highway Bridges

	STANDARDS - BRIDGES AND STRUCTURES (BD SERIES)
BD 41/97	Reinforced Clay Brickwork Retaining Walls of Pocket Type and Grouted Cavity type Construction Use of BS 5628: Part 2: 1995
BD-42/00	Design of Embedded Retaining Walls and Bridge Abutments
BD-43/03	The Impregnation of Reinforced and Prestressed Concrete Highway Structures using Hydrophobic Pore-Lining Impregnants
BD-44/95	The Assessment of Concrete Highway-Bridges and Structures
BD-45/93	Identification Marking of Highway Structures
BD-46/92	Technical Requirements for the Assessment and Strengthening Programme for Highway Structures [Stage 2 - Modern Short Span Bridges]
BD 47/99	Waterproofing and Surfacing of Concrete Bridge Decks
BD-48/93	The Assessment and Strengthening of Highway Bridge Supports
BD-49/01	Design Rules for Aerodynamic Effects on Bridges
BD 50/92	Technical Requirements for the Assessment and Strengthening Programme for Highway Structures Stage 3 - Long Span Bridges
BD-51/98	Portal and Cantilever Signs/Signal Gantries
BD 53/95	Inspection and Records for Road Tunnels
BD 54/93	Post-tensioned Concrete Bridges, Prioritisation of Special Inspections
BD 56/96	The Assessment of Steel Highway Bridges and Structures
BD 57/01	Design for Durability
BD-58/94	The Design of Concrete Highway Bridges and Structures with External and Unbonded Prestressing Design of Highway Bridges for Vehicle Collision Loads
BD 60/04	Design of Highway Bridges for Vehicle Collision Loads
BD-61/96	The Assessment of Composite Highway Bridges
BD-62/07	As Built, Operational and Maintenance Records for Highway Structures
BD 63/07	Inspection of Highway Structures
BD 65/97	Design Criteria for Collision Protector Beams
BD 67/96	Enclosure of Bridges
BD-68/97	Crib-Retaining-Walls
BD-70/03	Strengthened/Reinforced Soils and Other Fills for Retaining Walls and Bridge Abutments Use of BS8006: 1995, incorporating Amendment No. 1 (Issue 2 March 1999)
BD 74/00	Foundations
BD 78/99	Design of Road Tunnels
BD 79/06	The Management of sub Standard Highway Structures
BD-81/02	Use of Compressive Membrane Action in Bridge Decks
BD-82/00	Design of Buried Rigid Pipes
BD-84/02	Strengthening of Concrete Bridge Supports Vehicle Impact Using Fibre Reinforced Polymers
BD-85/08	Strengthening Highway Structures Using Externally Bonded Fibre Reinforced Polymer
BD-86/07	The Assessment of Highway Bridges and Structures For The Effects of Special Types General Order (STGO) and Special Order (SO) Vehicles
BD-87/05	Maintenance Painting of Steelwork

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	STANDARDS - BRIDGES AND STRUCTURES (BD SERIES)
BD 89/03	The Conservation of Highway Structures
BD-90/05	Design of FRP Bridges and Highway Structures
BD-91/04	Unreinforced Masonry Arch Bridges
BD-94/07	Design-of-Minor-Structures
BD-95/07	Treatment of Existing Structures on Highway-widening-Schemes
	TECHNICAL MEMORANDA - BRIDGES (BE SERIES)
BE-13	Fatigue Risk in Bailey Bridges
BE-23	Shear-Key-Decks-Amendment-No. 1 to Annex
BE 5/75	Rules-for-the-Design-and-Use-of-Freyssinet-Goncrete-Hinges-in-Highway-Structures
BE-7/04	Departmental Standard (Interim)
	Motorway Sign/Signal Gantries
	INTERIM ADVICE NOTES (IAN)
IAN 117/08 Rev 1	Certification of combined kerb and drainage products
IAN-116/08	Nature conservation advice in relation to bats
IAN 104/07	The Anchorage of Reinforcement and Fixings in Hardened Concrete
IAN-97/07	Assessment and upgrading of existing parapets
IAN 96/07r1	Guidance on implementing Results of Research on Bridge Deck Waterproofing
IAN 95/07	Revised Guidance Regarding the Use of BS8500(2006) For the Design and Construction of Structures Using Concrete
IAN-91/07	Interim Advice on the identification of "Particularly at Risk" supports
IAN 70/06	Implementation of New Reinforcement Standards
IAN 69/05	Design for Maintenance
IAN 48/03	Measures To Minimise The Risk of Sulphate Attack (Including Thaumasite) - New Construction and Structures Under Construction
IAN 47/02	Post Tensioned Grouted Duct concrete Bridges
IAN 41/02	European Cement Standards
IAN 05/96	BD 24/92 The Design of Concrete Highway Bridges and Structures. Use of BS 5400:

BD-44/95 The Assessment of Concrete Highway Bridges and Structures

BA 50/93 Post Tensioned concrete Bridges

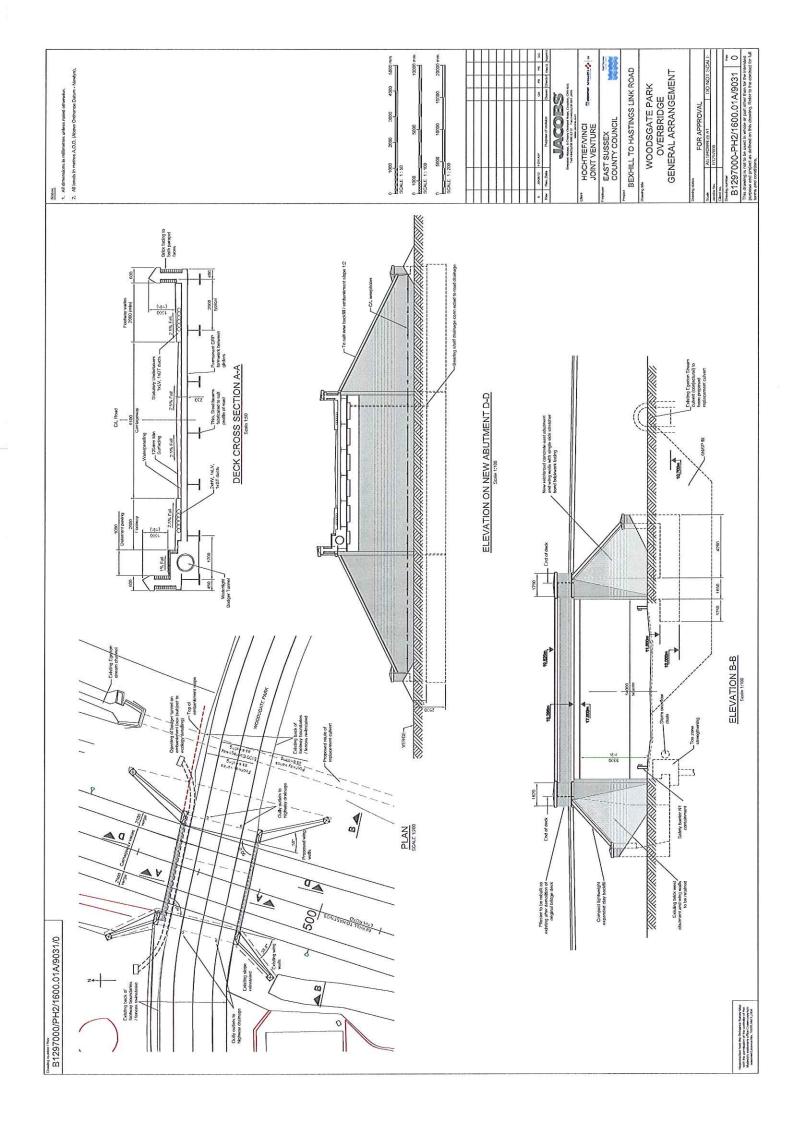
Part 4:1990

IAN 04/96

IAN 03/96

Appendix B Drawings

Drawing No B1297000-PH2/1600.01a/9031 Title S03 Woodsgate Park overbridge AIP General Arrangement



Appendix C Geotechnical Information

STRUCTURE NAME	CHAINAGE and OS Grid Re	eference	
S03 - Woodsgate Park Overbridge	Ch 520 OS: 5739	43E,108529N	
Rev: 1	DESIGN LIFE: 120 years		
SOILS/GEOLOGY	RELEVANT TRIAL HOLES: BH1, BH2, BH3, BH4 (ESCC Investigation, 1992)		
Strata	Typical depths		
Made Ground Alluvium Tunbridge Wells Sand Formation	18.65 to 11.25m OD 11.25 to 8.75m OD Below 8.75m OD		
PREVIOUS GROUND HISTORY	Railway cutting, brownfield site		
CONTAMINATED GROUND RISK AS	SSESSMENT REQUIRED	TBC	

GROUNDWATER

Groundwater strike was recorded at 8.35m OD (10.30m bgl) in BH1 and BH2 within the Tunbridge Wells Sand Formation. In BH3 and BH4 groundwater strike was recorded at 11.20m OD (7.5m bgl) within the Alluvium layer. No rise was recorded in any of the boreholes. No monitoring results are available. Allowing for seasonal fluctuations, the preliminary design groundwater level is assumed to be at 10.20m OD (6.5m bgl).

EARTH PRESSURE VALUE Ko* Ka* Kp*

Refer to section 5.4 of the AIP.

TYPE OF FOUNDATION	Spread footing for East Abutment. Toe strengthening works in the front of the existing West Abutment will be founded on piles.			
BEARING CAPACITY	Spread footing for East abutment.			
Structure Element	Founding Stratum	Founding Level (m OD)	Footing Size	Allowable Bearing Pressure (kN/m2)
East Abutment and wingwall	Fill (6N)	10.0	12.0 x 7.60m (abutment) 9.80 x 7.60 (wingwalls)	200

PILE DESIGN: Toe strengthening works in the front of the existing west abutment.					
Structure Element	Founding Stratum	Toe Level (mOD)	Pile dia (m)	Pile length (m)	Pile working Load (kN)
West abutment and wingwall	Tunbridge Wells Sand Formation	5.0	0.45	5.0	TBC

Note: Pile lengths and toe levels are approximate – pile cap elevations to be confirmed.

Pile type: CFA / Bored

Criteria for selecting pile toe level: Pile capacity

Allowance for negative skin friction within design:

SETTLEMENT

Differential settlement to be allowed for between adjacent supports: 25mm

Differential settlement to be allowed between structure and approach embankment: 20mm

(within 10m of the interface between structures and approach embankment)

CHEMICAL ANALYSIS

Buried Concrete classification:

The results of chemical tests on soil samples taken within the urban areas indicate pH values ranging between 3.68 and 10.5 and sulfates (2:1 Water Extract) values of between 10 mg/l and 1150 mg/l. The recommended Design Sulfate and Concrete Classification based on BRE Special Digest 1 (2005) are DS-2 and AC4z respectively.

NOTES

- Elevation was not shown on the borehole logs. The levels have been estimated from the ESCC long section drawing (No. 262701\090047 Fieldwork Location Plan and Geological Long Section Sheet 1 of 4).
- 2. The ground sequence at the site is Made Ground, Alluvium and Tunbridge Wells Sand. Based on the foundation level (10m OD), the structure is likely to be founded on the soft Alluvium. Made Ground and Alluvium are not recommended as a bearing stratum due to its unpredictable bearing behaviour and poses a risk of differential settlement taking place. The maximum thickness of Made Ground is 7.4m and the maximum thickness of Alluvium is 2.3m.
- It is recommended that the foundations of the structure is founded on the Stiff to very stiff /very dense interbeded sands, silts and clays of the Tunbridge Wells Sand at a minimum level of 8.75m OD
- 4. The soft Alluvium beneath the foundation will need to be excavated and replaced with suitable structural fill material. The depth of excavation is likely to be 1.5m below formation level. Due to likelihood of encountering groundwater, the recommended backfill material is Class 6A below groundwater level and Class 6N/6P above the groundwater level
- 5. The excavated foundation will need to be inspected for the presence of any widened fissures.

EAST SUSSEX COUNTY COUNCIL
Highways & Transportation - Soils and Materials Group

Borehole No. BH1 Job No. CW1257 Sheet 1 of 2

Dates		Coordinates			Site BEXHILL NORTHERN APPROACH ROAD		
13/01/92 - 14/01/92		E N					
Method		Ground Level			Client DESIGN AND CONSTRUCTION		
Shell & A	uger.			mOD			
Depth m	Sumpl/Test	Field Records	level mOD	Depth m (Thick)	Description	Logend	
				(0.50)	ROAD PAVEMENT CONSTRUCTION		
				(0.30)	Firm mottled brown/grey sandy clay with granite chips		
1.00 - 1.50 1.00 - 1.50	U 1 (26 BLOHS)			(0.30)			
1.50 - 2.00 1.50 - 2.00 1.50 - 2.00	SPT N(O) SJ 3 B 4	0,0/0,0,0		ահատաահո			
2.50 - 3.00 2.50 - 3.00	U 5 (30 BLOWS)						
3.00 - 3.50 3.00 - 3.50 3.00 - 3.50	SPT N(9) SJ 7 B 8	1,1/2,2,2,3		(4.60)	Firm to stiff orange brown clayey silt with fragments of sandstone, siltstone, chalk and brick (FILL)		
4.00 - 4.50 4.00 - 4.50	U 9 (44 BLOWS) J 10			(4.60)			
4.50 - 5.00 4.50 - 5.00 4.50 - 5.00	SPT N(8) SJ 11 B 12	1,2/2,2,2,2		աասաև			
		13/01/92:DRY			я	*****	
5.50 - 6.00 5.50 - 6.00	U 13 (31 BLOWS)	14/01/92:DRY		5.40			
6.00 - 6.50 6.00 - 6.50 6.00 - 6.50	SPT N(15) SJ 15 B 16	1,2/3,3,4,5		(1.50)	Firm to stiff grey mottled black slightly organic silty clay with some flint pebbles and fragments of rotting wood (FILL)		
7.00 - 7.50 7.00 - 7.50	U 17 (40 BLOWS) J 18			6.90			
7.50 - 8.00 7.50 - 8.00 7.50 - 8.00	SPT N(4) SJ 19 B 20	1,1/1,1,1,1		(2.30)	Firm to stiff olive grey mottled black slightly organic silty CLAY with fragments of rotted wood and black amorphous silty PEAT layers	1 1/V H 1/V N N N N N N N N N N N N N N N N N N N	
				(2.30)	(ALLUVIUM)	- JVA	
8.50 - 9.00 8.50 - 9.00	U 21 (14 BLOWS) J 22				(1000)	.W. = .W.	
9.00 - 9.50 9.00 - 9.50 9.00 - 9.50	SPT N(40) SJ 23 B 24	1,2/5,8,12,15		9.20		رالاد_ « درالاد_ «	
9.50 - 10.00 9.50 - 10.00	1			9.20 E (1.00)	Very stiff thickly laminated light grey SILT with occasional orange ironstaining (TUNBRIDGE WELLS SAND)		
10.00 - 10.50		NO PENETRATION	<u></u>	<u>F</u>		Scale	
Remarks	Casing to 7.5m					1:50	
						lossed	
l					281092/1101	NAA	

Highways & Transportation - Soils and Materials Group

Borehole No. BH1 Job No. CH1257

2 of 2 Sheet BEXHILL HORTHERN APPROACH ROAD Site Coordinates Dates N 13/01/92 - 14/01/92 E DESIGN AND CONSTRUCTION Client Ground Level Method Shell & Auger. Depth legend Description Depth Field Records Sampk/Test m (Thi=k) mOD (Continued) 10.20 10.50 - 11.00 SJ 27 10.50 - 11.00 SPT N(420*) 10.50 - 11.00 B 28 Very dense light grey fine SAND with clayey SILT laminations and occasional orange ironstaining (2.30)(TUNBRIDGE WELLS SAND) 12.00 - 12.50 SPT N(242*) 12.00 - 12.50 SJ 29 40,30/,,, 12,50 14/01/92:10.0 Seeb Remarks Casing to 7.5m No penetration and no recovery from U100 at 10.0m SPT's at 10.5m and 12.0m failed to reach test depth 1:50 logged 281092/1102 NAA

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See key sheet for symbols and abbreviations

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Highways & Transportation - Soils and Materials Group

Borehole No. BH2

Job No. CH1257

Sheet 1 of 2

Dates	1	Coordinates			Site BEXHILL NORTHERN APPROACH ROAD	
15/01/92 -	16/01/92	E		N	Client DESIGN AND CONSTRUCTION	
Method Shell & Au	ger.	Ground Level		mOD	Client DESIGN AND CONSTRUCTION	
Depth m	Sample/Test	FirM Records	lsval mOD	Depth m (Thick)	Description	Legend
				(0.50)	ROAD PAVEMENT CONSTRUCTION	
				E 0,50	CHALK rubble with flints	
	1) 4 (7/ PLOUE)			(0.40)	(FILL)	****
1.00 - 1.50	U 1 (34 BLOWS) J 2					****
1.50 - 2.00 1.50 - 2.00 1.50 - 2.00	SPT N(6) SJ 3 B 4	2,2/2,2,1,1				
2.50 - 3.00 2.50 - 3.00	U 5 (34 BLOHS)			(3.40)	Firm to stiff brown slightly clayey silt with siltstone fragments and orange ironstaining	
3.00 - 3.50 3.00 - 3.50 3.00 - 3.50	SPT H(14) SJ 7 B 8	2,2/3,3,4,4		ասաաանաև	(FILL)	
4.00 - 4.50 4.00 - 4.50	U 9 (39 BLOWS) J 10			4.30		
4.50 - 5.00 4.50 - 5.00	U 11 (73 BLOWS) J 12			mum.		
5.00 - 5.50 5.00 - 5.50 5.00 - 5.50	SPT N(12) SJ 13 B 14	2,3/3,2,4,3		4.30	Firm grey silty clay and silt with occasional brick fragments and orange ironststaining	
6.00 - 6.50 6.00 - 6.50	U 15 (43 BLOWS) J 16			(3.10)		
6.50 - 7.00 6.50 - 7.00 6.50 - 7.00	SPT N(9) SJ 17 B 18	2,1/3,1,2,3		7.40		
		4F 104 (02-DDV		7.40		
7.50 - 8.00 7.50 - 8.00	U 19 (16 BLOWS)	15/01/92:DRY 16/01/92:DRY	-			
	1410 170000	0,1/0,1,0,1				.\\\.\\\.\\\\\\\\\\\\\\\\\\\\\\\\\\\\\
8.00 - 8.50 8.00 - 8.50 8.00 - 8.50	SPT N(2) SJ 21 B 22			(2.00)	Soft dark grey/black clayey organic SILT with decomposing wood and plant material	W.
9.00 - 9.50 9.00 - 9.50	U 23 (54 BLOHS)				(ALLUVIUM)	W.
9.50 - 10.00 9.50 - 10.00	U 25 (149 BLOWS) J 26			9.40		* * * * * * * * * * * * * * * * * * *
Remarks	Casing to 10.5m	<u></u>	J	- 9.90		Scab 1:50
						Logged
Sen buy sheet for	symbols and abbseviations				281092/1617	NAA

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EAST SUSSEX COUNTY COUNCIL Highways & Transportation - Soils and Materials Group

Borehole No. BH2 Job No. CW1257 Sheet 2 of 2

Dates		Coordinates			Site BEXHILL NORTHERN APPROACH ROAD	
15/01/92 -	16/01/92	Е		N		
Method Shell & Aug	ger.	Ground Level		mOD	Client DESIGN AND CONSTRUCTION	
Depth m	Sampb/Test	Fall Records	lewl mOD	Dopth tn (Thick)	Description	lege
10.50 - 11.00 10.50 - 11.00 10.50 - 11.00	SJ 27 SPT N(64*) B 28	STRIKE at 10.3m 19,14/18,25,7,		1.90)	(Continued) Very dense light grey very fine SAN with occasional orange ironstaining (TUNBRIDGE WELLS SAND)	
	U 29 (161 BLOWS)	F F (42 24 47		11.80		X X X X X X X X X X X X X X X X X X X
12.50 - 13.00 12.50 - 13.00 12.50 - 13.00	SPT N(58*) SJ 31 B 32	5,5/12,21,17,	e	(2,70)	Very stiff grey clayey SILT with siltstone fragments (TUNBRIDGE WELLS SAND)	* * * * * * * * * * * * * * * * * * *
14.00 - 14.50 14.00 - 14.50 14.00 - 14.50	SPT N(173*) SJ 33 B 34	37,17/,,,		14.50		, , , , , , , , , , , , , , , , , , ,
3				արվարումարուժուսակարուհայանարակարուկարումարում (արդակարում		
Remarks	Casing to 10.5m SPT at 14.0m failed	d to reach test de	pth			Scat
						logg

Highways & Transportation - Soils and Materials Group

Borehole No. Job No.

Sheet

BH3 cu1257 1 of 2

BEXHILL NORTHERN APPROACH ROAD Site Coordinates Dates N 22/01/92 - 24/01/92 DESIGN AND CONSTRUCTION Client Ground Level Method Shell & Auger, mOD Depth legend Description Depth Fell Pecods Sample/Test (Thick) mOD ROAD PAVEHENT CONSTRUCTION (0.50)0.50 Firm brown silty clay with flints (FILL) (0.40)0.90 1.00 - 1.50 U 1 (26 BLOWS) Soft light grey slightly clayey silt with fragments of siltstone, flint and organic material and occasional orange ironstaining (FILL) 1,1/1,1,1,1 1.50 - 2.00 1.50 - 2.00 1.50 - 2.00 (1.80)U 5 (34 BLOWS) 2.50 - 3.00 2.70 SPT N(7) SJ 7 B 8 3,2/1,2,3,1 3.00 - 3.50 3.00 - 3.50 3.00 - 3.50 Firm laminated mottled grey light grey/ brown mudstone and silt with brick fragments and occasional orange ironstaining U 9 (24 BLOWS) 4.00 - 4.50 (2.60)(FILL) 2,1/2,1,2,1 SPT H(6) SJ 11 B 12 4.50 - 5.00 4.50 - 5.00 4.50 - 5.00 5.30 U 13 (19 BLOWS) 5.50 - 6.00 Firm orange clayey silt and fine SAND with fragments of blast furnace slag 1,1/1,1,3,2 SPT N(7) SJ 15 B 16 6.00 - 6.50 6.00 - 6.50 6.00 - 6.50 (1.50) (FILL) 6.80 U 17 (29 BLONS) 7.00 - 7.50 7.00 - 7.50 W Very soft black/dark brown slightly fibrous clayey PEAT W 0,0/0,0,0,0 STRIKE at 7.5m 7.50 - 8.00 7.50 - 8.00 7.50 - 8.00 SPT N(0) SJ 19 B 20 Ņ٧. W. (1.60)NI (ALLUVIUM) 22/01/92:6.0 alle. 23/01/92:7.9 U 21 (125 BLOWS) 8.40 8.50 - 9.00 SPT N(31) SJ 23 B 24 4,6/8,9,6,8 9.00 - 9.50 9.00 - 9.50 9.00 - 9.50 Very stiff interbedded grey slightly clayey SILT and fine SAND 1,2/2,3,2,2 9.50 - 10.00 9.50 - 10.00 9.50 - 10.00 SPT N(9) SJ 25 B 26 (TUNBRIDGE WELLS SAND) 10.00 - 10.50 U 27 (166 BLOWS) Remarks Casing to 12.0m 1:50 Logged 281092/1109 NAA

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See my sheet for symbols and abbreviations

Highways & Transportation - Soils and Materials Group

Borehole No. BH3
Job No. cu1257
Sheet 2 of 2

Dates	gyant abytis is as	Coordinates			Site BEXHILL HORTHERN APPROACH ROAD	
22/01/92	- 24/01/92	Б		N		
Method		Ground Level			Client DESIGN AND CONSTRUCTION	
Shell & Au	uger.		, ,	mOD Depth	D. John	legend
Depth m	Sample/Test	Firld Records	lowl mOD	m (lásídl)	Description	X · Y · X
10.00 - 10.50	J 28			1	(Continued)	* * * * * * * * * * * * * * * * * * *
10.50 - 11.00 10.50 - 11.00 10.50 - 11.00		4,6/6,8,6,12		ահասաս		
11.00 - 11.50 11.00 - 11.50 11.00 - 11.50	C000	5,10/16,26,8,		ասա		1
11.50 - 12.00 11.50 - 12.00	SJ 33 B 34			dum		
12.00 - 12.50 12.00 - 12.50 12.00 - 12.50	SPT N(185*) SJ 35 B 36	10,16/34,,,		m.l.		
12.50 - 13.00 12.50 - 13.00 12.50 - 13.00	}	20,30/,,,		(8.60)		X X X X X X X X X X X X X X X X X X X
13.00 - 13.50 13.00 - 13.50 13.00 - 13.50	SPT N(*) SJ 39 B 40	23/01/92:8.0		1	Very stiff interbedded grey slightly clayey SILT and fine SAND	** * * * *
13.50 - 14.00 13.50 - 14.00 13.50 - 14.00	Districted Contractors	24/01/92:8.0 22,28/,,,		8.60)	(TUNBRIDGE WELLS SAND)	# # # # # # # # # # # # # # # # # # #
14.00 - 14.50 14.00 - 14.50 14.00 - 14.50		28,22/,,,		سسبل		
14.50 - 15.00 14.50 - 15.00 14.50 - 15.00	1	11,11/14,15,18,3		سسسل		* * * * * * * * * * * * * * * * * * *
15.00 - 15.50 15.00 - 15.50 15.00 - 15.50	and the second of the second o	10,18/10,		հատա		
15.50 - 16.00 15.50 - 16.00 15.50 - 16.00	I .	12,15/18,27,5,		ասասա		*****
16.00 - 16.50 16.00 - 16.50 16.00 - 16.50	SPT N(71*) SJ 51 B 52	10,14/15,23,12,		- -		4 H H
16.50 - 17.00 16.50 - 17.00 16.50 - 17.00	SPT N(97*) SJ 53 B 54	14,17/20,26,4,		dumm		1
		24/01/92:8.0	-	17.00		1
	ľ					
				manadamandamandamandamandamandamandaman		
				in the	1	
				<u></u>		
				աստահատուս	1	
Remarks	Casing to 12.0m SPT's at 12.5m, 13	5.0m, 13.5m and 14	Om fai	_E	ach test depth	Scale 1:50
						logged
See key sheet for	symbols and abbreviations		p/21		281092/1110	HAA

Highways & Transportation - Soils and Materials Group

Borehole No. BH4

Job No. CW1257

Sheet 1 of 2

Dates		Coordinates			Site BEXHILL HORITICKH APPROACH ROAD	
20/01/92 -	21/01/92	Е		N	ATOTAL AND CONSTRUCTION	
Method Shell & Aug	ger.	Ground Level		mOD	Client DESIGN AND CONSTRUCTION	
Depth m	Samph/Tost	Field Records	Leval mOD	Depth m (Thick)	Dracription	legend
				(0.30)	ROAD PAVEMENT CONSTRUCTION	· · · · · · · · · · · · · · · · · · ·
				(0.60)	Brick and flint fragments in silty clay matrix (FILL)	
1.00 - 1.50	U 1 (35 BLOWS)			0.90		
1.50 - 2.00 1.50 - 2.00 1.50 - 2.00	SPT N(10) SJ 3 B 4	1,1/2,2,3,3		աևառավա		
2.50 - 3.00 2.50 - 3.00	U 5 (44 BLOWS)			modenna		
3.00 - 3.50 3.00 - 3.50 3.00 - 3.50	SPT N(10) SJ 7 B 8	2,3/2,2,3,3		աստակաստանությունապատանուս		
4.00 - 4.50	U 9 (52 BLOWS) J 10	0.2m RECOVERED		(6.00)	Firm light grey clayey silt with fragments of siltstone brick and flint with occasional orange ironstaining	
4.50 - 5.00 4.50 - 5.00 4.50 - 5.00	SPT N(11) SJ 11 B 12	1,3/2,2,3,4		ահասաահա	(FILL)	
5.50 - 6.00 5.50 - 6.00	U 13 (30 BLOWS)			mandanandanandanandanandanandanandanand		
6.00 - 6.50 6.00 - 6.50 6.00 - 6.50	SPT N(5) SJ 15 B 16	1,1/1,1,2,1 20/01/92:DRY				
7.00 - 7.50 7.00 - 7.50	U 17 (30 BLOWS) J 18	21/01/92:DRY		6.90		J., W.
7.50 - 8.00 7.50 - 8.00 7.50 - 8.00 7.50 - 8.00	SPT N(4) SJ 19 B 20	1,1/1,1,1,1 STRIKE at 7.5m		1.80)	Soft dark brown/black slightly fibrous silty PEAT with rotting wood	. W. . W. . W. . W.
8.50 - 9.00	U 21 (40 BLOWS) J 22			ահատա	(ALLUVIUM)	.WW.
9.00 - 9.50 9.00 - 9.50	J 22 U 23 (136 BLOWS) J 24			8.70	Stiff to very stiff light grey very silty CLAY with occasional orange ironstaining	×
9.50 - 10.00 9.50 - 10.00 9.50 - 10.00	SPT N(173*)	20,30/,,,		9.40	1	***
Remarks	Casing to 9.0m SPT at 9.5m failed	d to reach test de	.pth	<u> </u>		Scab 1:5
	of the Fish fatter	- 	om 0			Logge

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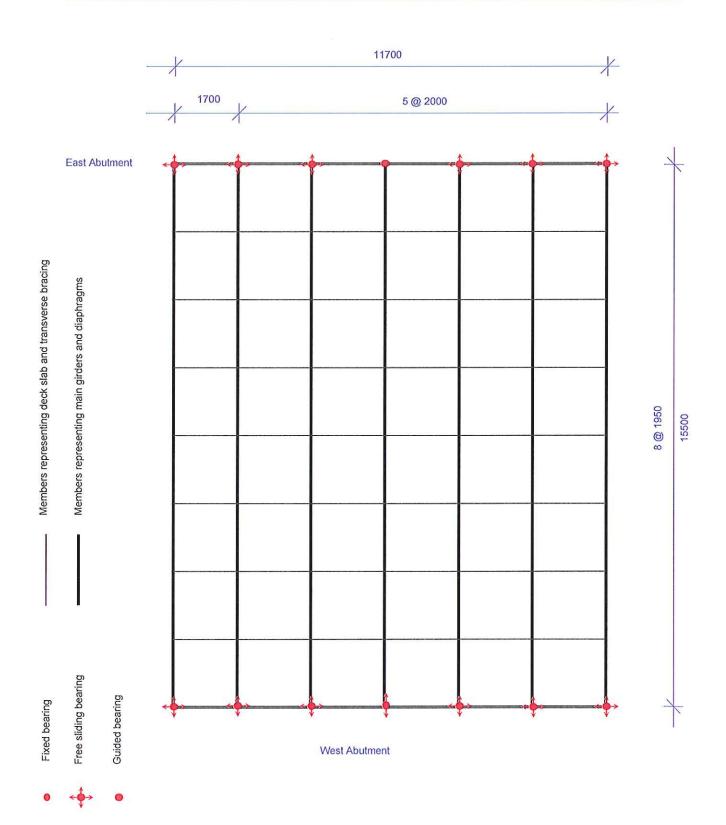
Borehole No. BH4

Job No. CW1257

Sheet 2 of 2

Dates		Coordinates	<u> </u>		Site BEXHILL HORTHERN APPROACH ROAD	
20/01/92 -	21/01/92	Е		N	The selection	
Method Shell & Au		Ground Level		αOD	Client DESIGN AND CONSTRUCTION	
Depth	Sample/Test	Fell Records	Lavel mOD	Depth m	Description	legend
11.00 - 11.50 11.00 - 11.50 12.50 - 13.00 12.50 - 13.00 12.50 - 13.00 14.00 - 14.50 14.00 - 14.50	SPT N(50) SJ 27 B 28 SPT N(150*) SJ 29 B 30	628/4,14,10 10,40/,,, 50,/,,, 21/01/92:10.0		(b) (5.10)	light grey fine SAND With Sittstone fragments (TUNBRIDGE WELLS SAND)	Scalo
Remarks	Casing to 9.0m SPI's at 12.5m ar	nd 14.0m failed to	reach	test depti	i	1:50
						by
See hav sheet fo	r symbols and abbreviations				281092/1112	NAA

Appendix D Idealised Structure



Appendix E Departures from Standards

Departure D3: Verges over/under Structures

Nature of Departure

A standard verge width of 2.5m has been applied along the scheme mainline. Where the mainline crosses over an underbridge, or under an overbridge, it has been decided to reduce the verge width to provide associated cost savings on structure construction. Verge widths will also be reduced on sideroads and accommodation works structures. The verges will be reduced to the minimum allowed, while ensuring necessary Stopping Sight Distance is maintained. The verge width will be tapered to the reduced width over an acceptable distance. Where verge widening has been provided around bends to maintain SSD these verges will not be minimised.

Reason for Departure

This departure is sought to minimise construction costs for the structures by minimising the necessary deck width. This departure is requested as the DMRB Standards require the verge width to be continuous and maintained over/under all structures. This leads to excessive structure widths which are uneconomical.

Mitigation Factors

There are no pedestrian facilities over any of the mainline structures so verge reduction will not impact NMUs in the majority of cases. On the accommodation overbridges, there will only be a minor usage, and the likelihood of NMUs coming into conflict with farm vehicles is minimal. In addition, these departures are only requested over short distances over/under structures.

Implications for Safety

Though a reduced verge width will mean vehicles running closer to either the abutments or parapets, a safe minimum required width will be provided. Where deemed necessary as a result of the RRRAP assessment, vehicle barriers will be installed to reroute any errant vehicles away from the parapets or abutments.

